

Casting Simulation for Diesel Engine Flywheel by using Computer Aided Design and Manufacturing

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Abstract – Casting is one of the old procedures done on metals. Many products are formed using this method. The casting process like sand casting process which are the oldest casting process since 1950. The texture of the product depends upon the sand used for casting. The final product should be smooth at the end. Usually iron, steel, brass, aluminium, magnesium alloys are used to manufacture the flywheel. In this project, the S-Glass composite material is used to cast the Diesel Engine Flywheel. In this project, includes the CAD technologies combined with process simulation tools are increasingly used to optimize the filling and solidification of cast parts. This project describes the newly developed simulation of flywheel component via casting route. Results of the casting trails showed a high level of confidence in the simulation CAD and CAM tools.

Index Terms – Casting Simulation, flywheel, Shrinkage, Solidification.

1. CHAPTER I

Casting is one of four types: sand casting, permanent mold casting, plaster casting and Die casting. All these types of castings have their own advantages and disadvantages. Depending on the properties of the product required, one of the casting is selected.

Sand Casting: Sand casting is the oldest casting of the above. This method of casting is in use since 1950. The texture of the product depends on the sand used for casting. The end product is given smooth finishing at the end. Usually iron, steel, bronze, brass, aluminium, magnesium alloys which often include lead, tin, and zinc are used.

Permanent mold casting: Permanent mold casting uses two pieces of mold. This molds are joined together and molten metal is pored into this mold. The hot metal is allowed to cool and the mold pieces are separated. Some products have metal

extrusion which are removed by flash grind or by hand. Tin, lead and Zinc are commonly moulded using this method.

1.1 DIE CASTING

Die casting is a metal casting process that is characterized by forcing molten metal under high pressure into a mold cavity, which is machined into two hardened tool steel dies. Most die castings are made from non-ferrous metals, specifically zinc, copper, aluminium, magnesium, lead, pewter and tin based alloys. Depending on the type of metal being cast, a hot- or cold-chamber machine is used.

The casting equipment and the metal dies represent large capital costs and this tends to limit the process to high volume production. Manufacture of parts using die casting is relatively simple, involving only four main steps, which keeps the incremental cost per item low. It is especially suited for a large quantity of small to medium sized castings, which is why die casting produces more castings than any other casting process. Die castings are characterized by a very good surface finish (by casting standards) and dimensional consistency.

1.2 CAST METALS

The main die casting alloys are: zinc, aluminium, magnesium, copper, lead, and tin; although uncommon, ferrous die casting is possible. Specific dies casting alloys include: ZAMAK; zinc aluminium; aluminium to, e.g. The Aluminum Association (AA) standards: AA 380, AA 384, AA 386, AA 390; and AZ91D magnesium. The following is a summary of the advantages of each alloy:

Zinc: the easiest alloy to cast; high ductility; high impact strength; easily plated; economical for small parts; promotes long die life.

- Aluminium: lightweight; high dimensional stability for complex shapes and thin walls; good corrosion resistance; good mechanical properties; high thermal and electrical conductivity; retains strength at high temperatures.
- Magnesium: the easiest alloy to machine; excellent strength-to-weight ratio; lightest alloy commonly die cast.
- Copper: high hardness; high corrosion resistance; highest mechanical properties of alloys die cast; excellent wear resistance; excellent dimensional stability; strength approaching that of steel parts.
- Lead and tin: high density; extremely close dimensional accuracy; used for special forms of corrosion resistance. Such alloys are not used in foodservice applications for public health reasons.

1.3 EQUIPMENT

There are two basic types of die casting machines: *hot-chamber machines* and *cold-chamber machines*. These are rated by how much clamping force they can apply. Typical ratings are between 400 and 4,000 st (2,500 and 25,000 kg).

1.3.1 Hot-chamber machines

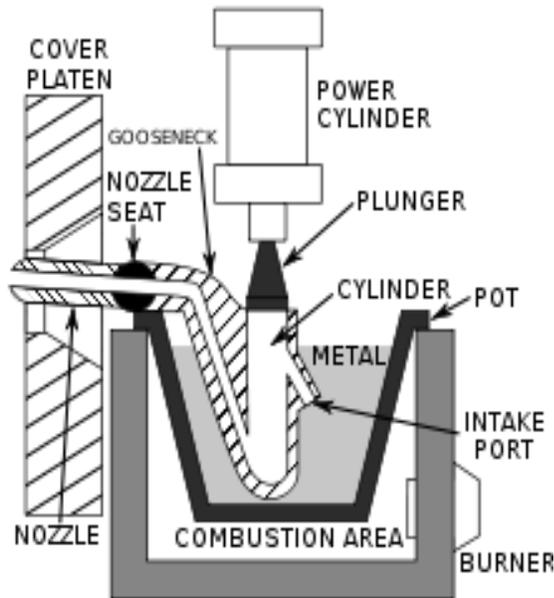


Fig:1 Schematic of a hot-chamber machine

Hot-chamber machines, also known as *gooseneck machines*, rely upon a pool of molten metal to feed the die. At the beginning of the cycle the piston of the machine is retracted, which allows the molten metal to fill the "gooseneck". The pneumatic or hydraulic powered piston then forces this metal out of the gooseneck into the die.

1.3.2 Cold-chamber machines

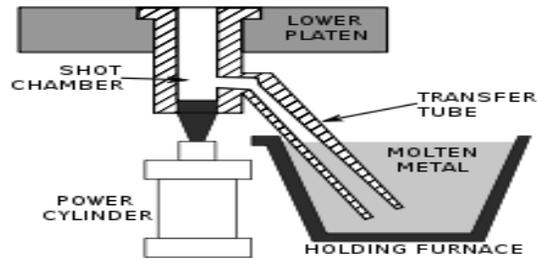


Fig:2 Cold-chamber die casting machine.

1.4 DIES

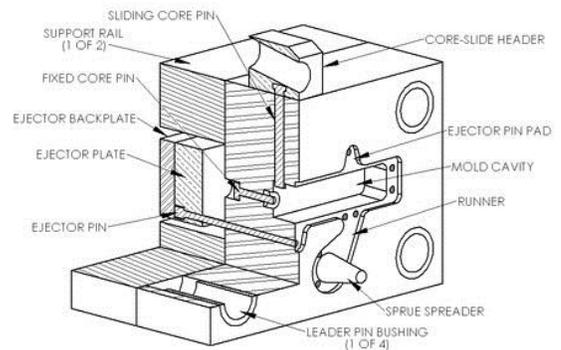


Fig: 3 The ejector die half

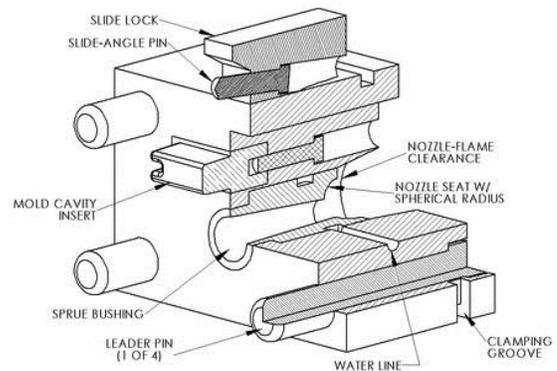
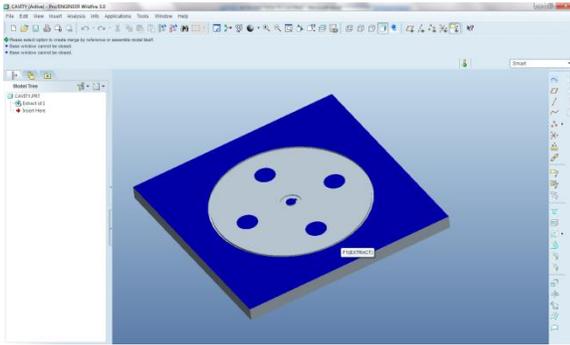


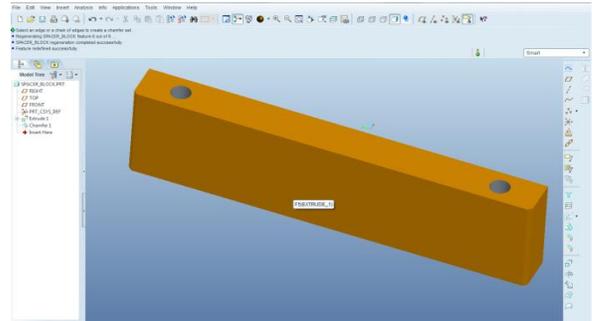
Fig:4 The cover die half

Two dies are used in die casting; one is called the "cover die half" and the other the "ejector die half". Where they meet is called the parting line. The cover die contains the sprue (for hot-chamber machines) or shot hole (for cold-chamber machines), which allows the molten metal to flow into the dies; this feature matches up with the injector nozzle on the hot-chamber machines or the shot chamber in the cold-chamber machines. The ejector die contains the ejector pins and usually the runner, which is the path from the sprue or shot hole to the mold cavity. The cover die is secured to the stationary, or front, platen of the casting machine, while the ejector die is attached to the movable platen. The mold cavity is cut into two *cavity*

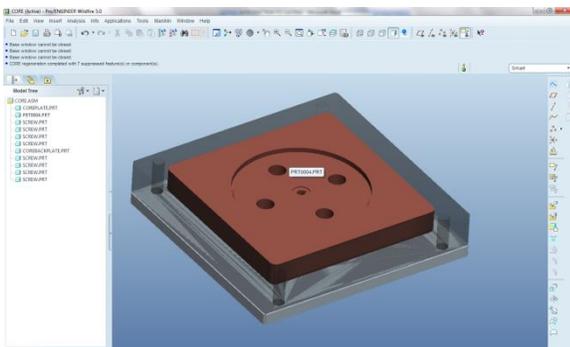
2.15 CAVITY



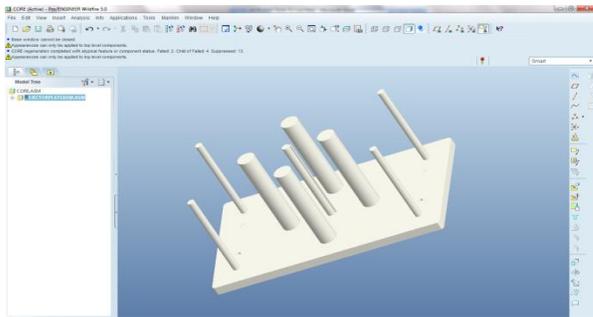
2.19 SPACER BLOCK



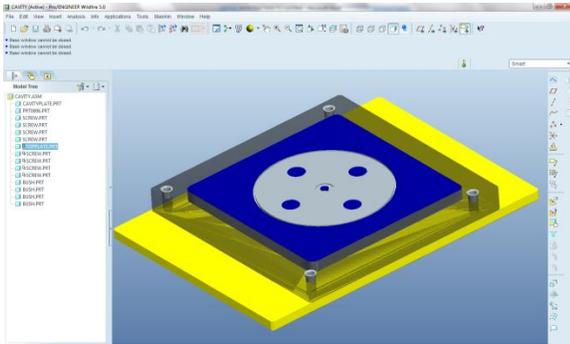
2.16 CORE AND BACK PALTE ASSEMBLY



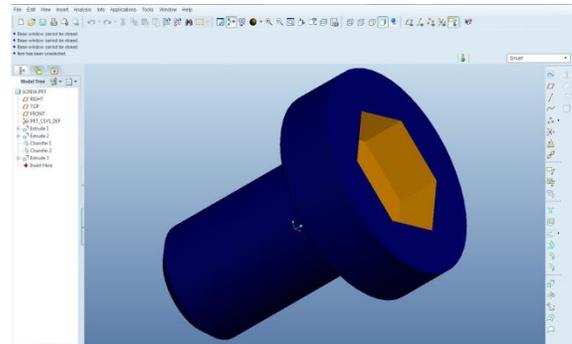
2.20 EJECTOR PLATE AND PINS



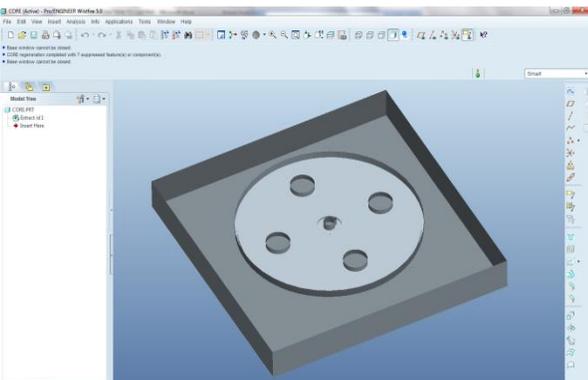
2.17 CAVITY AND TOP PLATE ASSEMBLY



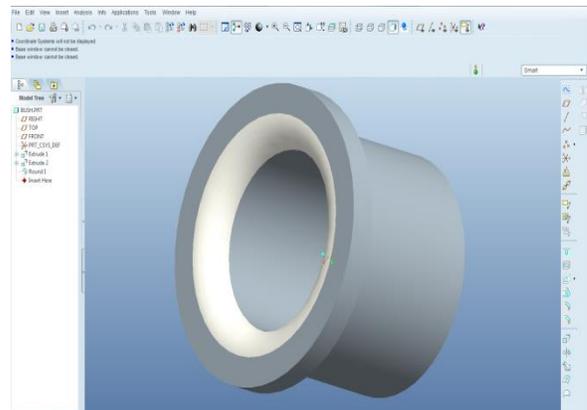
2.21 SCREW



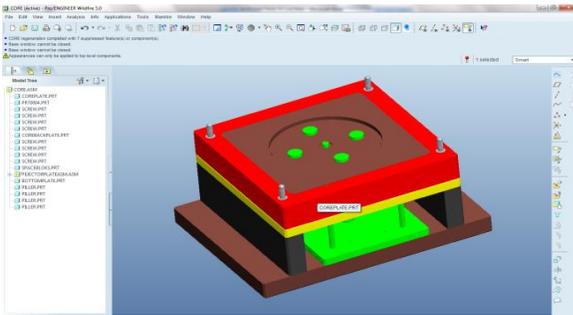
2.18 INSERT



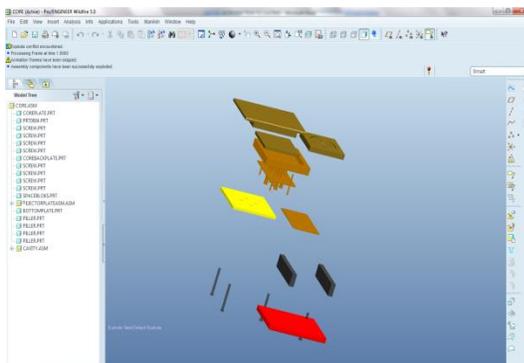
2.22 BUSH



2.23 CORE & CAVITY PARTIAL ASSEMBLY



2.24 EXPLODED VIEW



3. CHAPTER III

3.1 COMPUTER AIDED MANUFACTURING

Since the age of the Industrial Revolution, the manufacturing process has undergone many dramatic changes. One of the most dramatic of these changes is the introduction of Computer Aided Manufacturing (CAM), a system of using computer technology to assist the manufacturing process.

Through the use of CAM, a factory can become highly automated, through systems such as real-time control and robotics. A CAM system usually seeks to control the production process through varying degrees of automation. Because each of the many manufacturing processes in a CAM system is computer controlled, a high degree of precision can be achieved that is not possible with a human interface.

The CAM system, for example, sets the toolpath and executes precision machine operations based on the imported design. Some CAM systems bring in additional automation by also keeping track of materials and automating the ordering process, as well as tasks such as tool replacement.

Computer Aided Manufacturing is commonly linked to Computer Aided Design (CAD) systems. The resulting integrated CAD/CAM system then takes the computer-generated design, and feeds it directly into the manufacturing system; the design is then converted into multiple computer-controlled processes, such as drilling or turning.

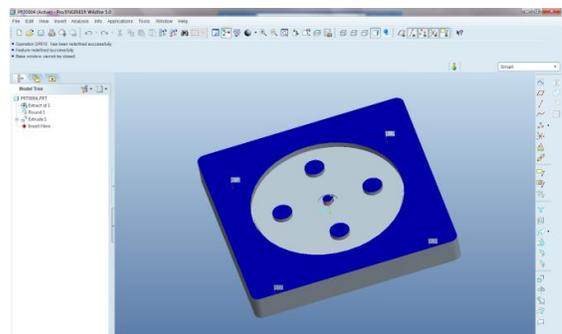
Another advantage of Computer Aided Manufacturing is that it can be used to facilitate mass customization: the process of creating small batches of products that are custom designed to suit each particular client. Without CAM, and the CAD process that precedes it, customization would be a time-consuming, manual and costly process. However, CAD software allows for easy customization and rapid design changes: the automatic controls of the CAM system make it possible to adjust the machinery automatically for each different order.

3.2 PROCEDURE OF MANUFACTURING

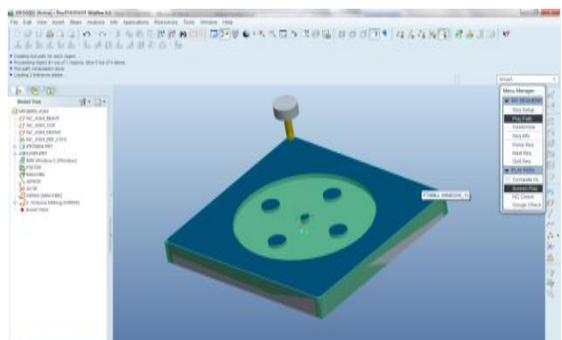
3.2.1 CAVITY

3.2.1 ROUGHING

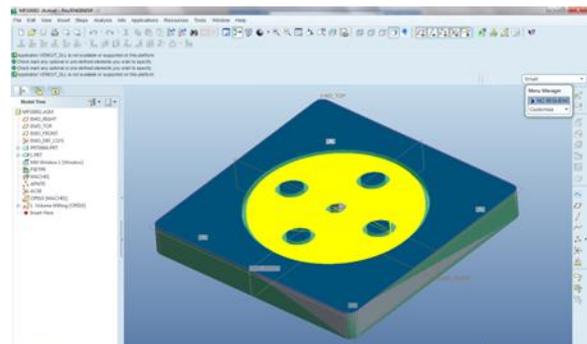
ROUGHING WITHOUT WORK PIECE



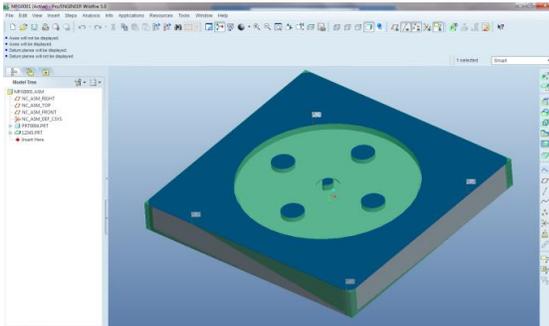
CUTTING TOOL



VERICUT



ROUGHING WITH WORKPIECE



X201.177

Y-29.57

X5.

Y-34.484

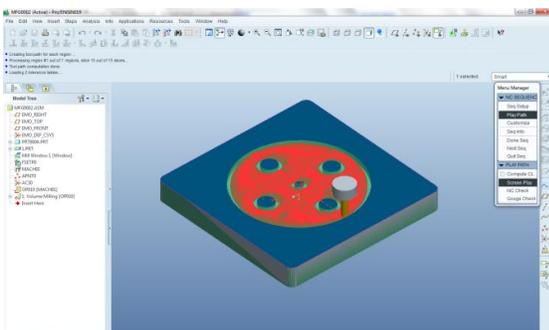
X201.177

Y-39.398

X5.

Y-44.313

PLAYPATH



X201.177

Y-49.227

X5.

Y-54.141

X201.177

Y-59.055

X5.

Y-63.969

X201.177

Y-68.883

4. CHAPTER IV

4.1 2 ROUGHING PROGRAM

%

G71

O0001

(D:\nsr\roughing.ncl.1)

N0010T1M06

S5000M03

G00X5.Y-5.

G43Z0.H01

G01Z-5.F200.

X201.177

Y-9.914

X5.

Y-14.828

X201.177

Y-19.742

X5.

Y-24.656

X5.

Y-73.797

X201.177

Y-78.711

X5.

Y-83.625

X201.177

Y-88.539

X5.

Y-93.453

X201.177

Y-98.367

X5.

Y-103.281

X201.177

Y-108.195

X5.

Y-113.109	G01X83.625
X201.177	X84.365Y-189.6
Y-118.023	G03X86.133Y-183.053I-11.24J6.547
X5.	G02X86.133Y-183.053I-13.008J0.
Y-122.938	G01Z0.
X201.177	G00X59.106
Y-127.852	Z-46.998
X5.	G01Z-51.006
Y-132.766	G03X64.097Y-193.778I14.019J0.
X201.177	G02X65.291Y-195.254I-3.22J-3.826
Y-137.68	X67.129Y-195.725I-.301J-4.991
X5.	G03X71.246Y-169.16I5.996J12.672
Y-142.594	G02X68.64Y-168.815I-.67J4.955
X201.177	G01X68.302Y-168.651
Y-147.508	X68.176Y-168.91
X5.	X67.875Y-169.383
Y-152.422	X67.524Y-169.82
X201.177	G02X66.26Y-170.83I-3.712J3.35
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X5.	G01Z-55.01
Y-162.25	X64.083
X201.177	G02X60.986Y-187.729I9.042J9.351
Y-167.164	G01X59.908
X5.	G02X59.106Y-183.053I13.217J4.676
Y-172.078	G01X60.117
X201.177	G02X60.986Y-178.377I13.008J0.
Y-176.992	G01X59.908
X5.	G02X62.68Y-173.701I13.217J-4.676
G01X85.164	G01X64.083
G02X86.131Y-182.865I-12.039J-4.926	G02X82.167Y-173.701I9.042J-9.352
G01X87.142	G01X83.569
X87.144Y-183.053	G02X86.341Y-178.377I-10.444J-9.352
G02X86.385Y-187.603I-14.019J0.	G01X85.263
G01X85.311	G02X86.133Y-183.053I-12.138J-4.676
G02X82.231Y-192.342I-12.186J4.55	G01X87.144

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G01X85.263

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G01X83.569

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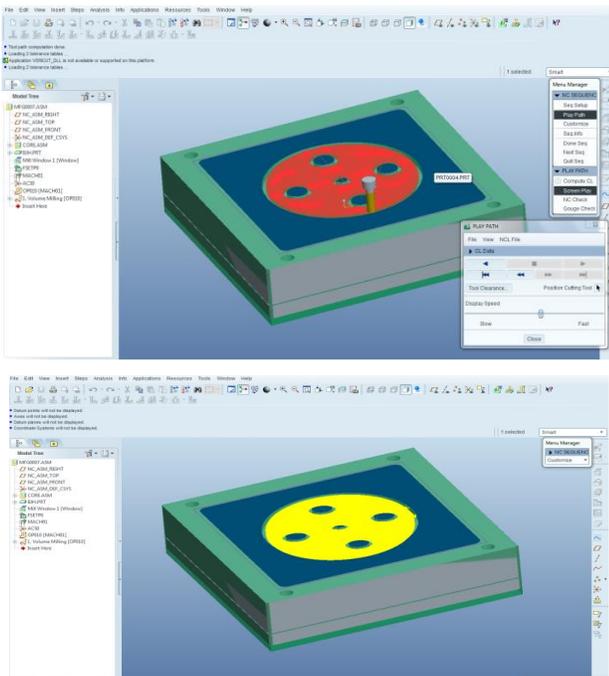
G03X87.144Y-183.053I-14.019J0.

G01Z0.

M30

%

4.2 FINISHING



4.2.1 PROGRAMME ON FINISHING

%

G71

O0002

(D:\nsr\finishing.ncl.1)

N0010T1M06

S5000M03

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G43Z0.H01

G01X111.522Y-140.847Z-1.753F200.

X112.214Y-142.226Z-2.34

X113.293Y-143.329Z-2.684

X114.657Y-144.05Z-2.874

X116.176Y-144.321Z-2.94

X116.284Y-144.322

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G02X119.694Y-146.003I0.J-4.3

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G03X123.348Y-146.411.865J1.433

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G03X124.226Y-168.252I3.203J1.849

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G03X124.157Y-173.425I3.202J1.849

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G01X120.181Y-176.772	X189.613Y-133.105
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G02X120.008Y-191.472I0.J-4.3	Z-108.266
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G03X124.45Y-193.713I3.724J2.15	X191.807Y-114.08
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X187.502Y-137.326	
X187.822Y-136.58	
X188.112Y-136.076	
X188.388Y-135.632	

5. CHAPTER V

5.1. CONCLUSION

By adopting the pressurized gating system, the fluid flow was smooth and air was expelled without any entrapment inside the mould cavity. Simulation showed that the molten metal was able to fill the mould within the desired time. Therefore fluid heat distribution was good and no cold shut was observed. In first iteration improper location of ingates led to formation of shrinkage porosities where in the second iteration only two ingates are located at the thicker section of the inner rib of the flywheel, on which risers are located in order to achieve directional solidification. The flywheel is manufactured using pressure die casting process for bulk production.

In this project the manufacturing process of flywheel (i.e) core-cavity extraction, total die parts and assembly, CNC program generation for core and cavity is done.

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